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Noise and vibration control in aerospace composite structures

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University of Toronto Institute for Aerospace Studies (UTIAS)

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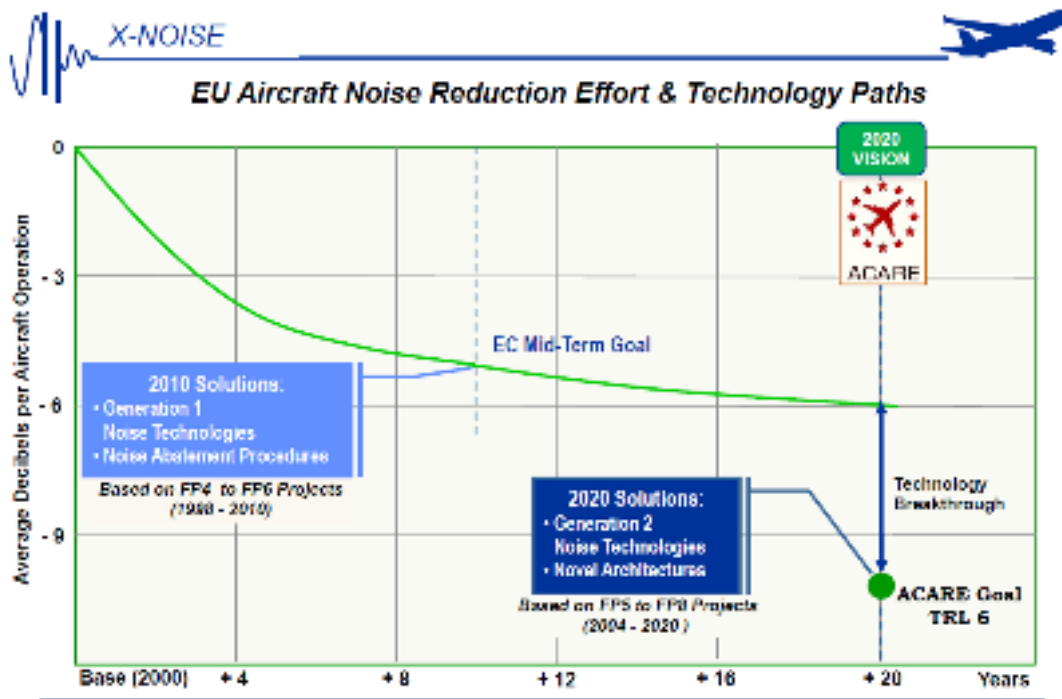
Fuel efficient engines and lighter structures



Reduced noise pollution around airports

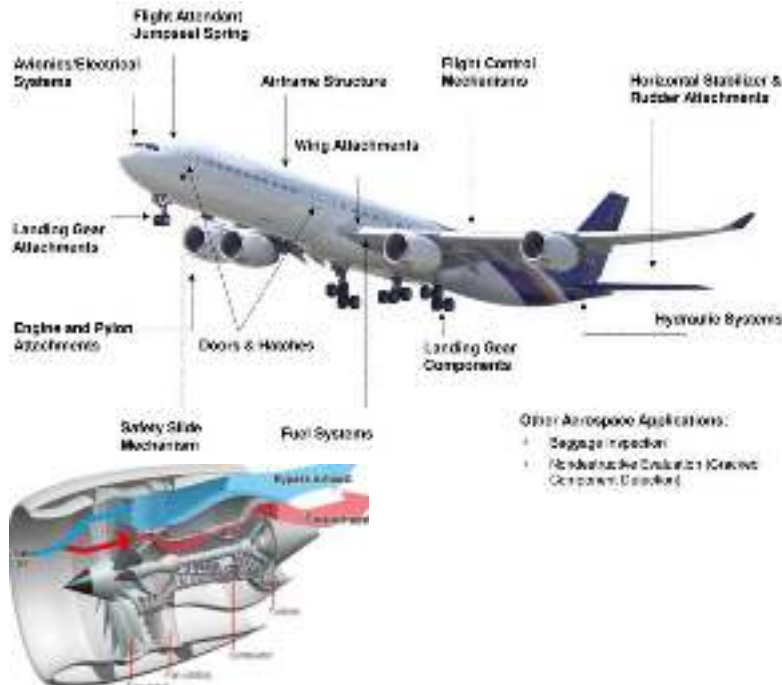


Acceptable noise and vibration levels inside aircraft cabins



Innovative solutions

- Intelligent use of added mass
- Increase structural damping
- Reduce noise level
- Reduce emissions
- Increase the payload



Aero Technologies LLC

Main noise and vibration sources in aircraft

- Engine (fan, turbine, jet)
- Interaction fluid-structure
- Hydraulic systems
- Landing gear

Structural vibrations

- Propagation through aircraft fuselage
- Propagation through flooring system

Structure-borne noise

- Transmission in solid structures (fuselage, flooring systems)
- Radiation from vibrating structures

Airborne noise

- Displacement of mass particles in the air (cabin)

Main objective: Reduce the noise and vibration level in aircrafts without detrimental impact on its composite structures

Acting on source



Reduced noise level

- Reduce noise level inside cabin
- Reduce noise annoyance to communities
- Mechanism: **Acoustic absorption**

Acting on media

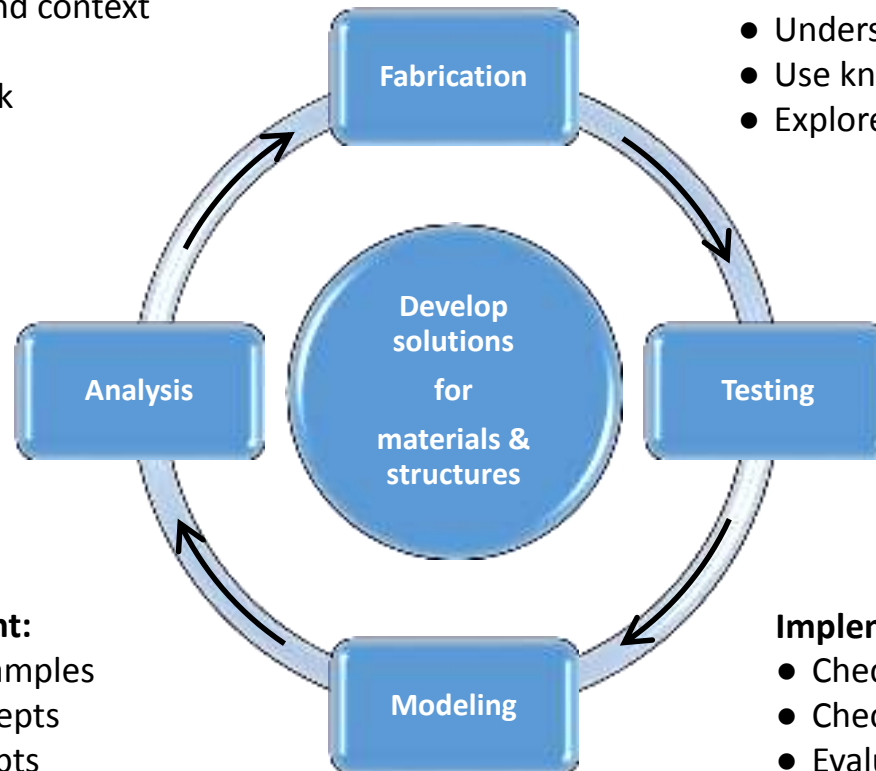


Reduced vibration level

- Reduce noise level inside cabin
- Increase structure durability
- Mechanisms: **Mechanical damping and acoustic transmission barrier**

Start from the beginning:

- Define the problem quantitatively
- Understand the needs and context
- Limit the domain
- Define statement of work
- Identify people
(Controlled goods)



Investigation:

- Define requirement specifications
- Understand technical parameters
- Use knowledge and expertise
- Explore innovative ideas

Small scale development:

- Fabricate lab demo samples
- Test preliminary concepts
- Select solution concepts
- Model concept and optimize
- Validate final concept

Implementation:

- Check for air worthiness
- Check for certification
- Evaluate impact on performance
- Develop integration procedures
- Complete proof of concept

NSERC-Safran chair on 3D composites for aerospace

Micro-characterization
thermosets

Mechanical and
dynamic testing

Manufacturing
and prototyping



DMA



MDSC



Pressclave with acquisition system



HP TGA-FTIR
spectrometer



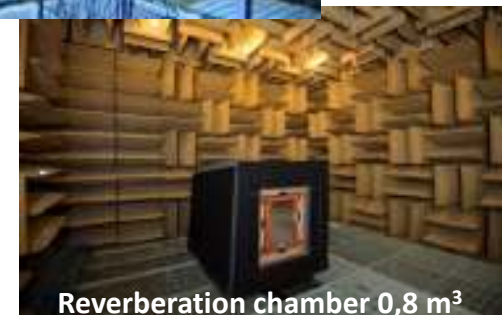
Rheometer



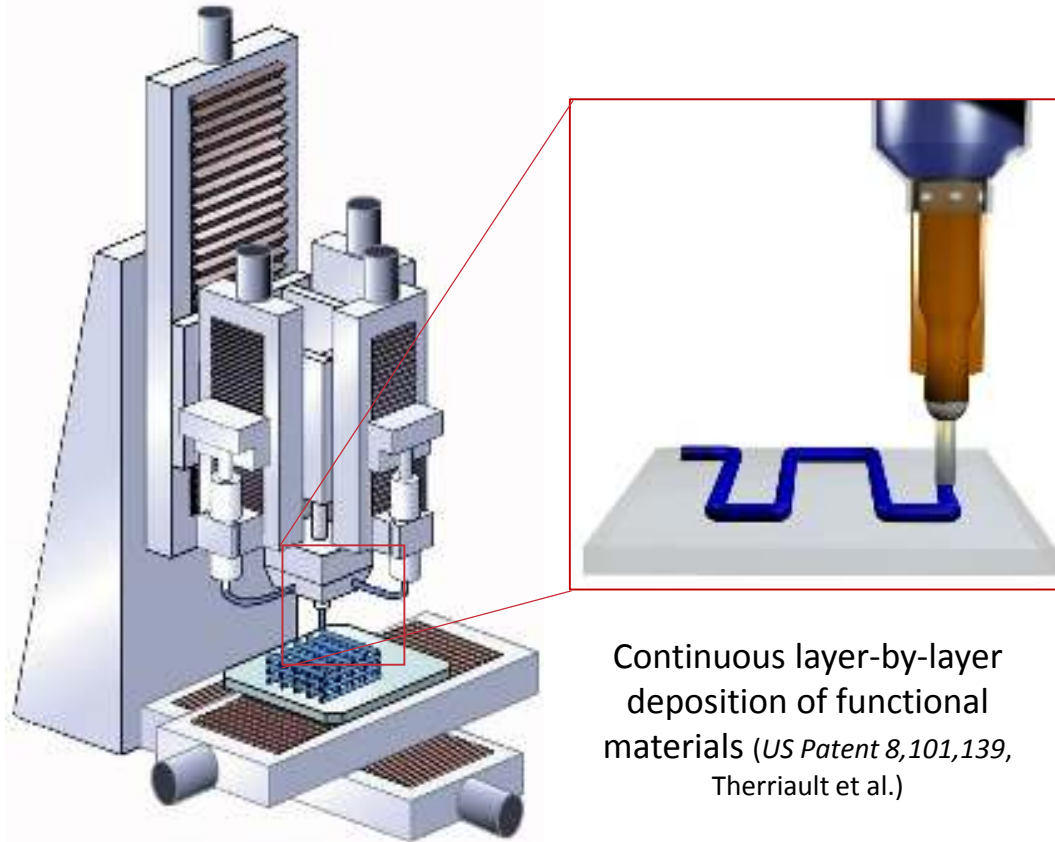
DMA-450 Metravib



Laboratory for acoustic and vibration analyses (LAVA)

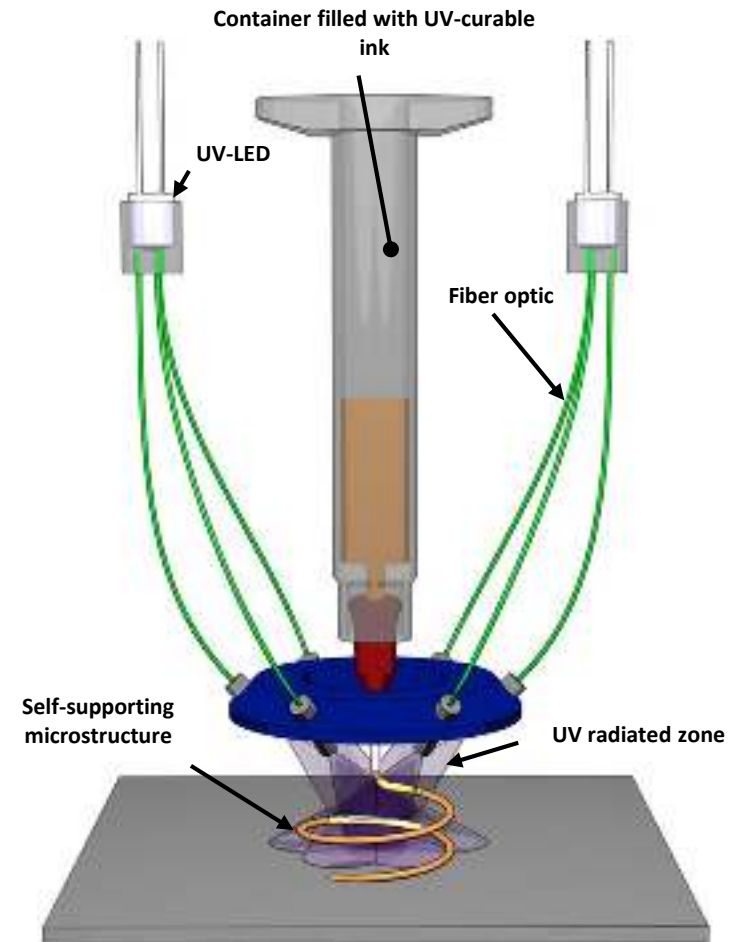


Laboratory of multiscale mechanics (LM2)



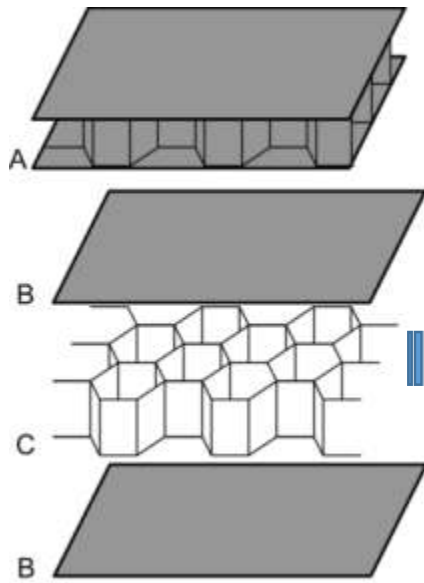
Continuous layer-by-layer
deposition of functional
materials (*US Patent 8,101,139*,
Therriault et al.)

3D printing of complex
microstructures
(Lewis, White, U of Illinois at Urbana-
Champaign)

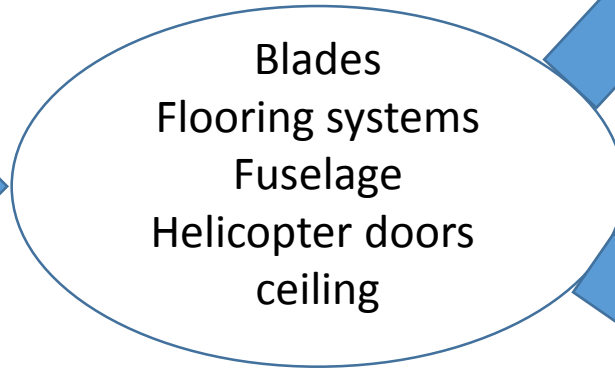


UV assisted freeform 3D printing
(L. Laberge Lebel)

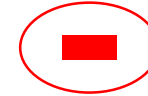
Motivations



Sandwich structure

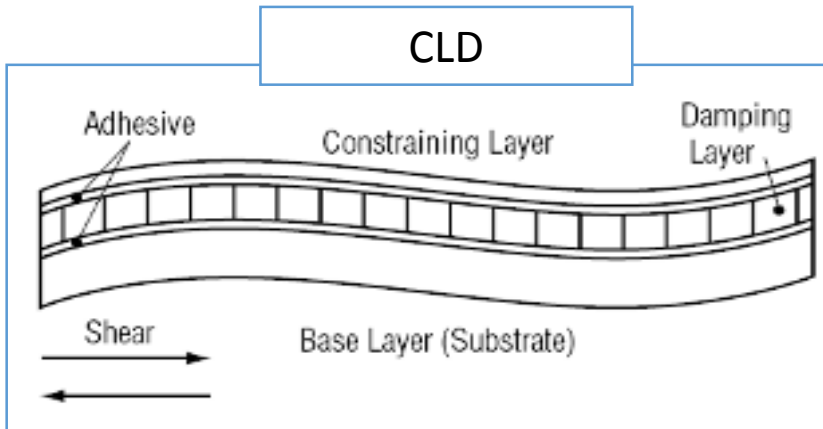


- High flexural stiffness/weight ratio
- Applications in transportation industry

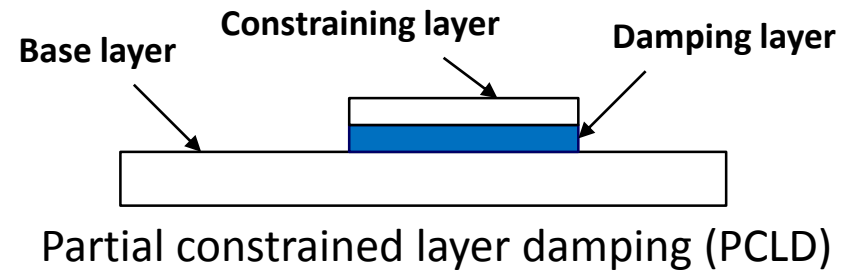


- Transmission of mechanical and acoustic vibrations
- Discomfort or mechanical damages

Passive damping



Constrained layer damping (CLD)



Shearing of viscoelastic material through flexural motion of the structure



Damping increase through energy dissipation

Passive damping (face sheets)

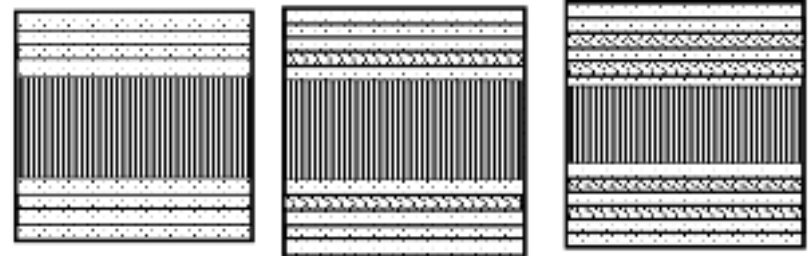
Composite prepreg



Viscoelastic material

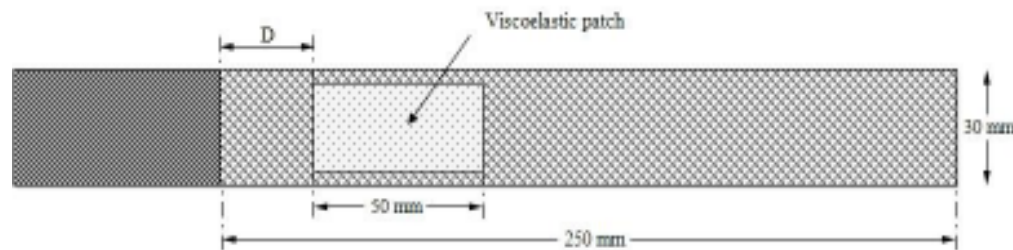


- Take advantage of the laminated structure of composite
- Interleaved viscoelastic material
- Insertion of viscoelastic material before curing
- Limited risk of delamination

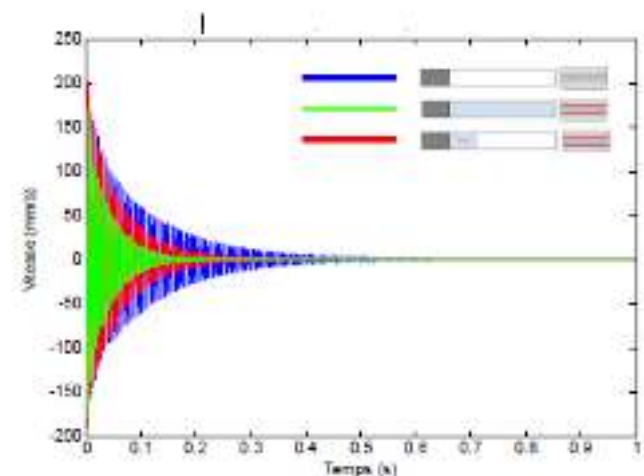


Carbon/epoxy layers Viscoelastic layers Honeycomb core

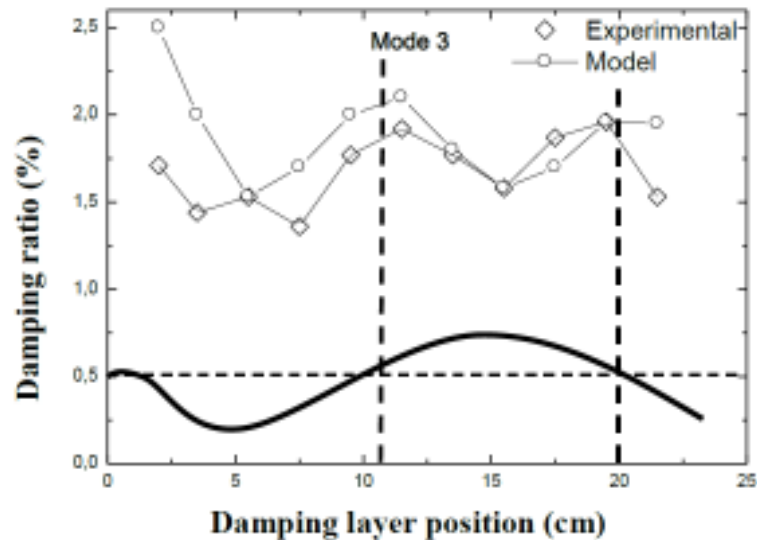
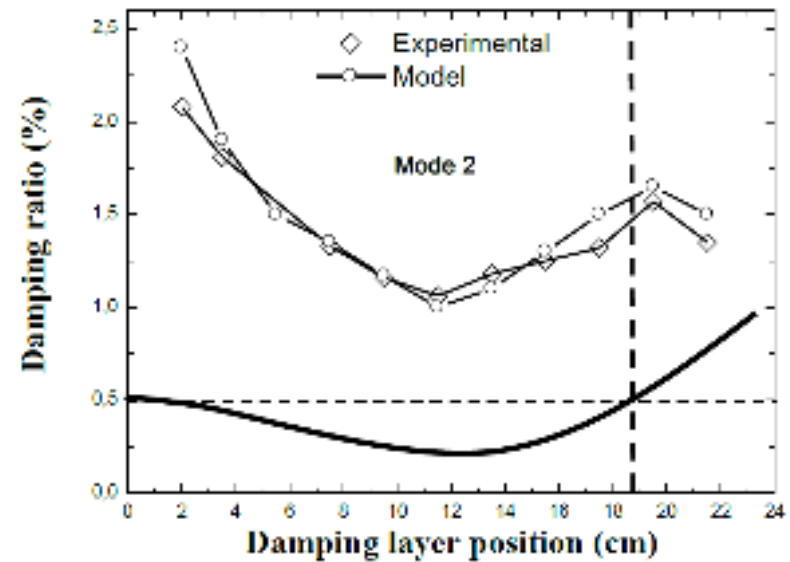
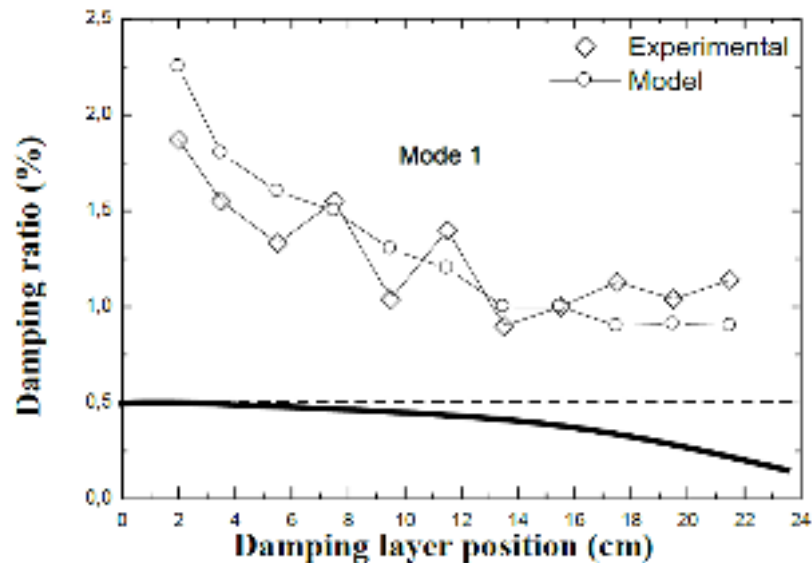
- Variable position viscoelastic material through the thickness
- Multiple shearing locations



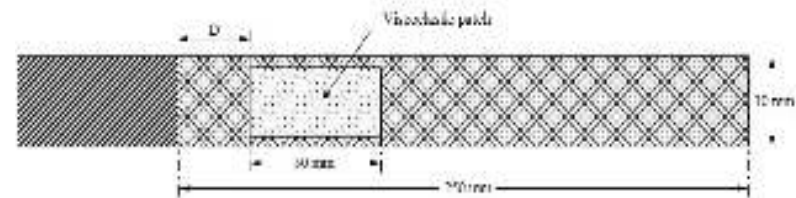
- Multiple positions along the structures
- Target areas of maximum deformation (modal node)



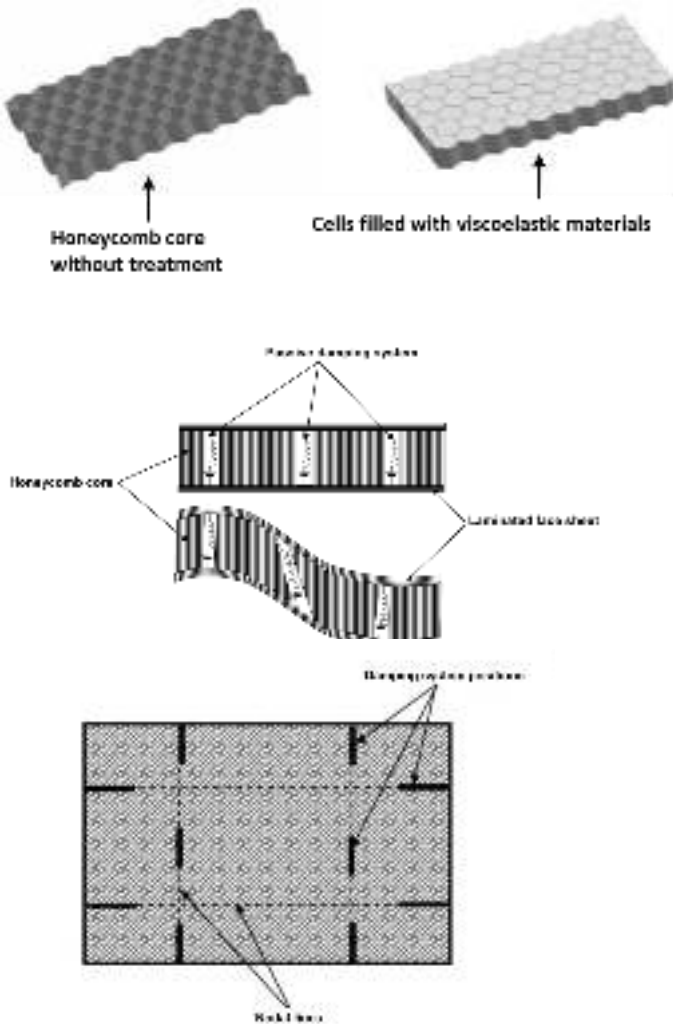
Experimental vs model



Increase of damping ratio at the modal nodes



Passive damping (core)



- Core stiffness modification
- Cells filled with viscoelastic materials
- Embedded damping device in the core
- Metamaterials in the core



Mapping of the whole structure along the nodal lines (high shear deformation)

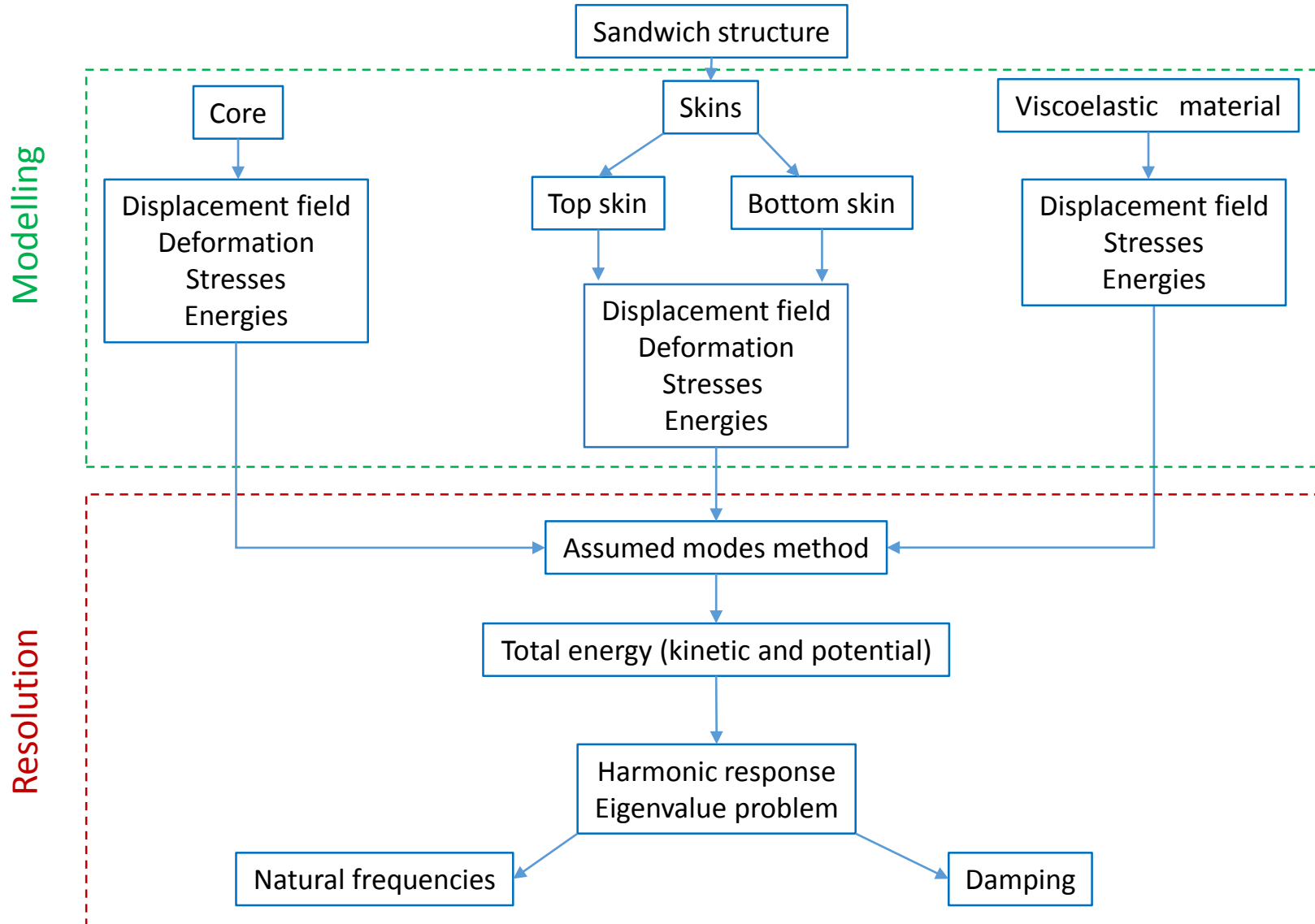


- Increase of structural damping
- Increase of acoustic transmission loss
- Reduction of the added mass



Risk of altering locally the mechanical properties of the structure

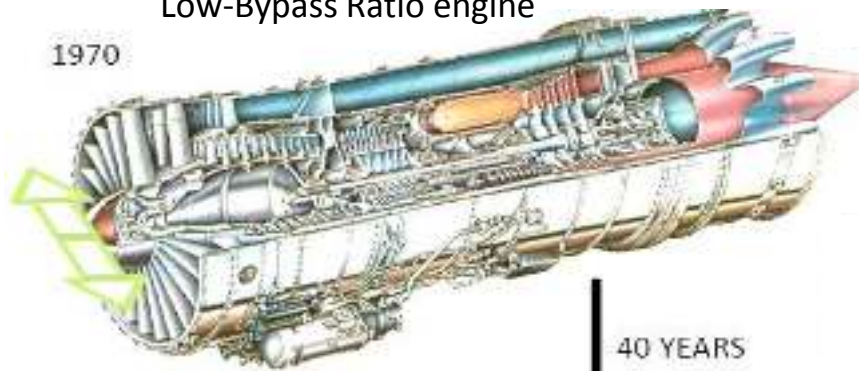
Modelling of passive damping



Motivations

Low-Bypass Ratio engine

1970

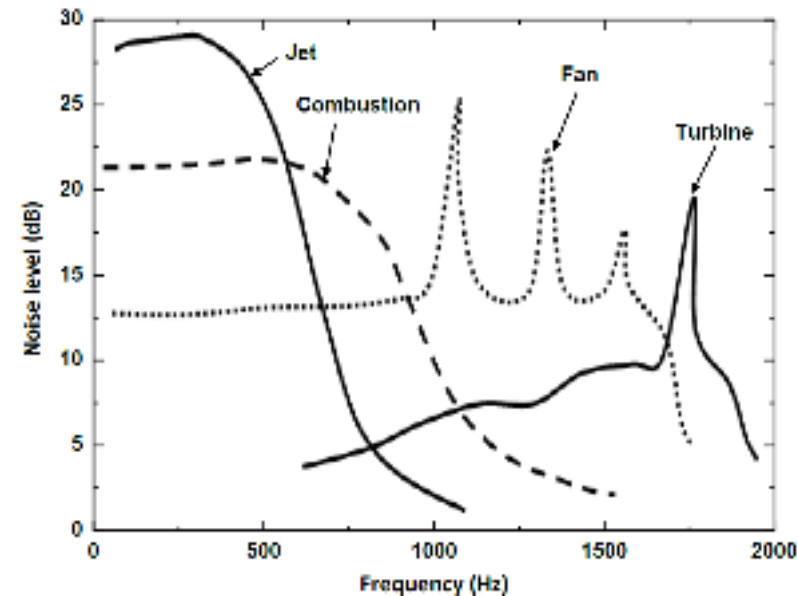


40 YEARS

2010



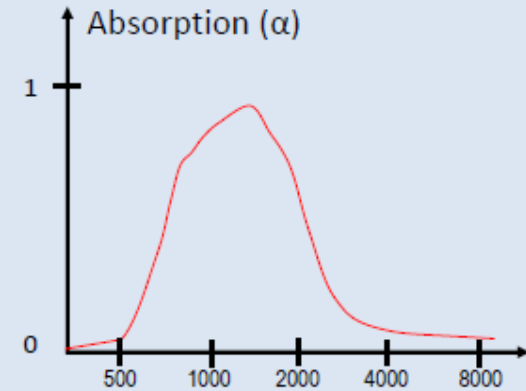
High-Bypass Ratio engine



- Several sources of noise
- Fan noise important during take-off and landing
- Annoyance to communities around airports
- Discomfort for passengers
- Reduced durability of the structures

- Engine length reduced
- Nacelle diameter increased
- Areas for acoustic treatment narrowed

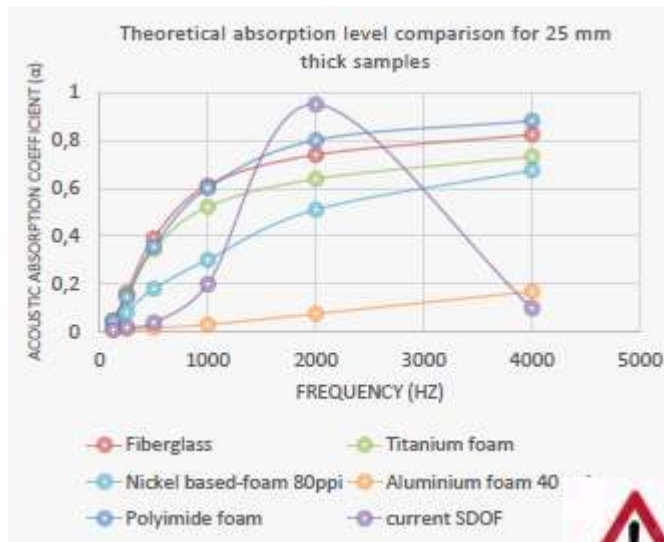
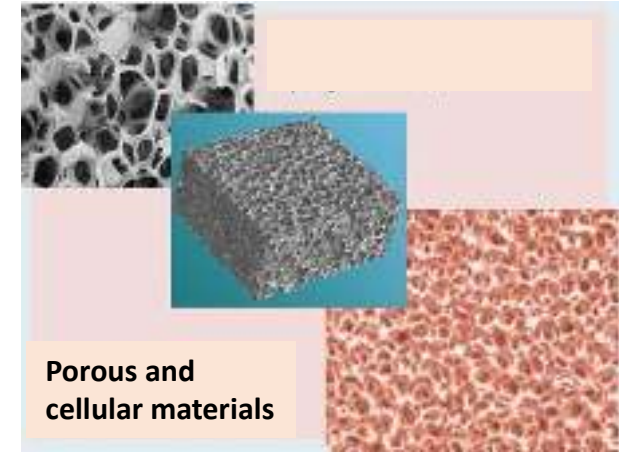
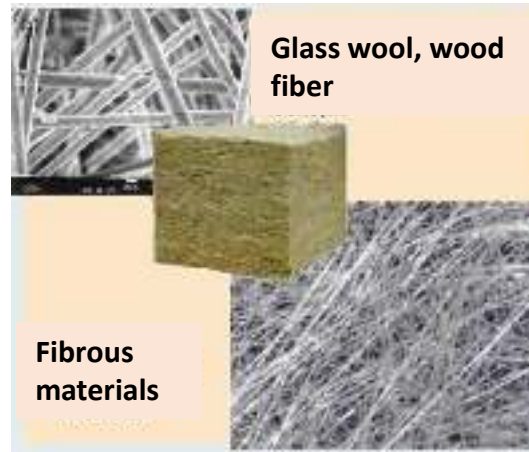
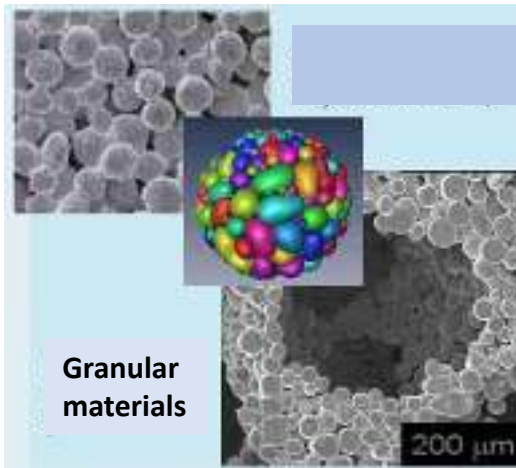
Locally reacting acoustic liner (Helmholtz resonators)



- Target only one octave band centered on fan blade passage frequencies
- Not suitable for critical areas such as OGVs
- Too cumbersome and heavy
- Development possibilities exhausted

- Need for new technologies breakthrough
- Development of new absorbing materials
- Development of new acoustic concepts
- Development of new integration procedures

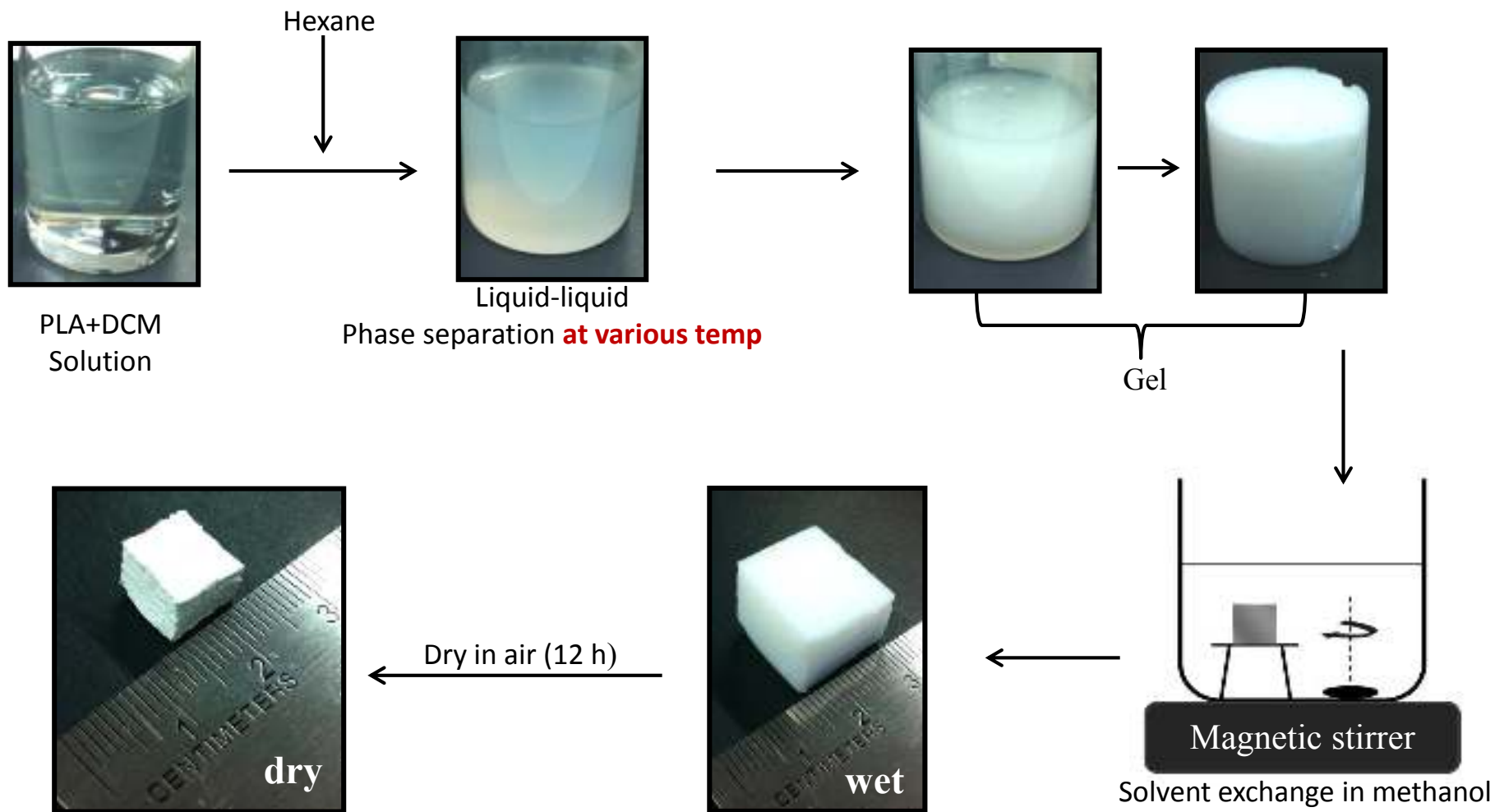
Non-locally reacting acoustic treatment



- High porosity metallic/carbon foams available
- Dissipation phenomena involved
- Broadband absorption frequency range
- Integration in composite environment
- Foaming processes difficult to control
- Foaming process expensive
- Mechanical behavior for high performance applications
- Ensuring long-term acoustic performance
- Certification compatibility

Foaming process PLA foams

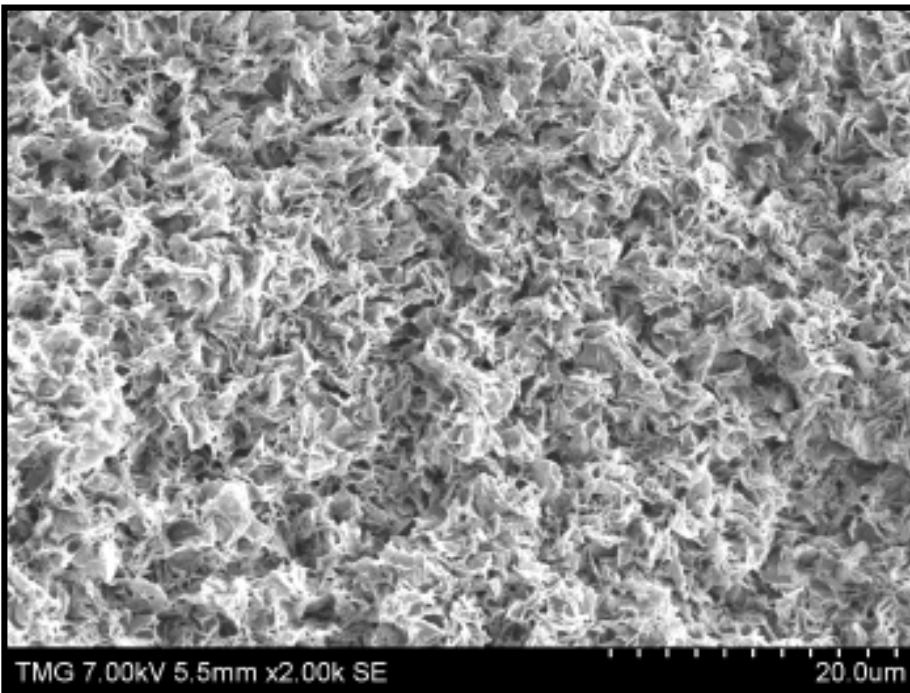
Non Solvent Induced Phase Separation (NIPS)



Microstructure PLA foams: Bimodal porosity

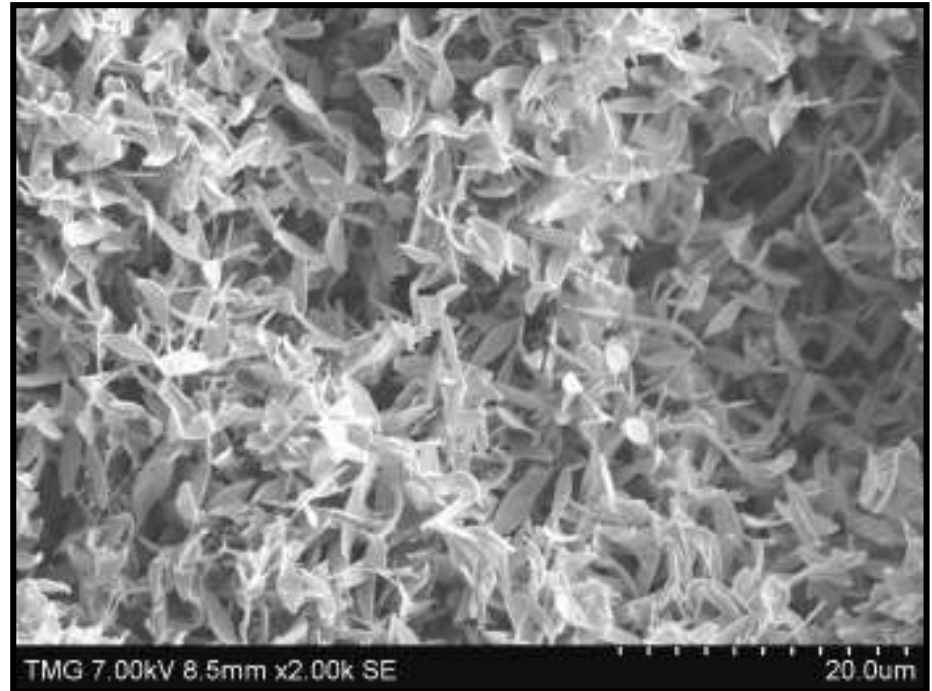
13 wt.% @ room temperature

23 wt.% @ room temperature



Porosity = 45%

Compressive Strength = 45 MPa

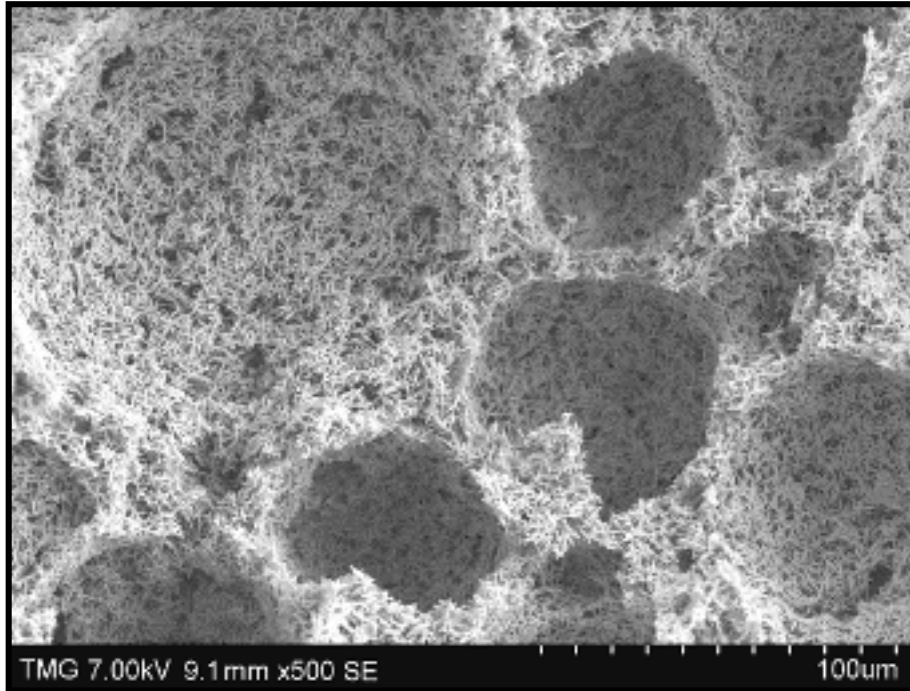


Porosity = 84%

Compressive Strength = 8 MPa

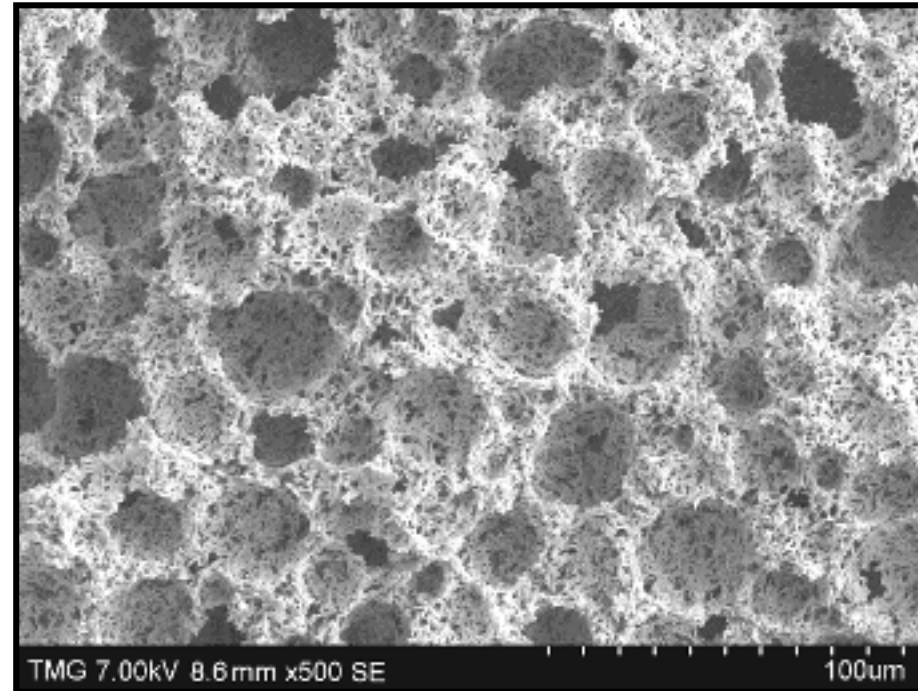
Microstructure PLA foams: Bimodal porosity

13 wt.% @ Freezer



Porosity = 91%
Compressive Strength = 1.8 MPa

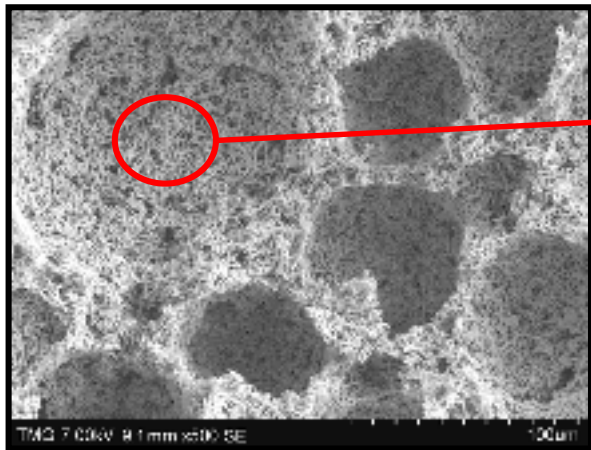
23 wt.% @ Freezer



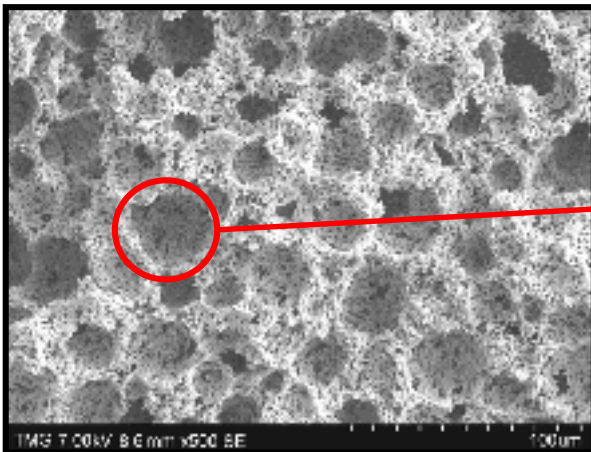
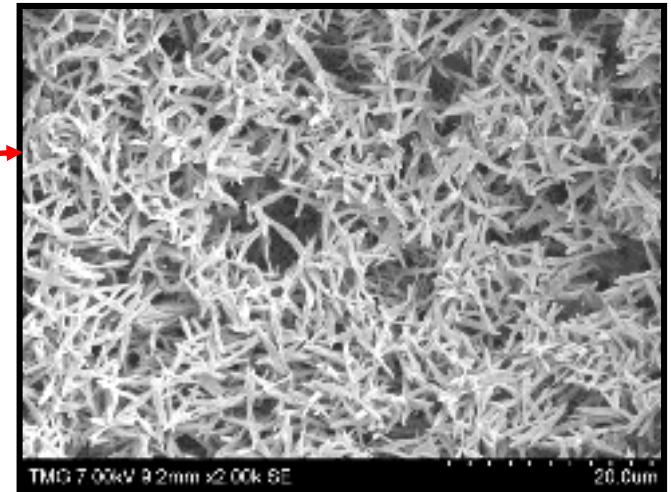
Porosity = 84%
Compressive Strength = 15.6 MPa

Nucleation & growth mechanism

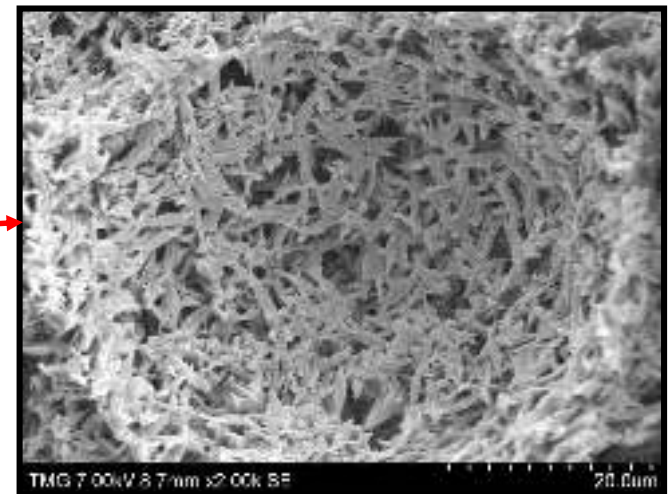
Microstructure PLA foams: Bimodal porosity



13 wt.% @ Freezer

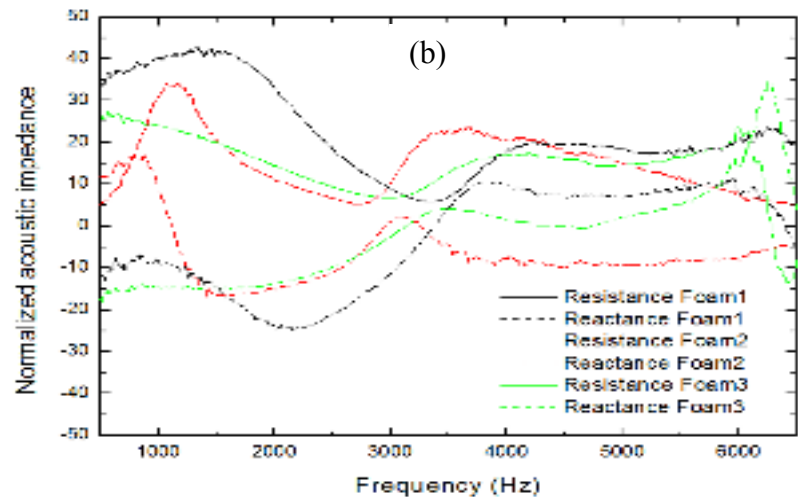
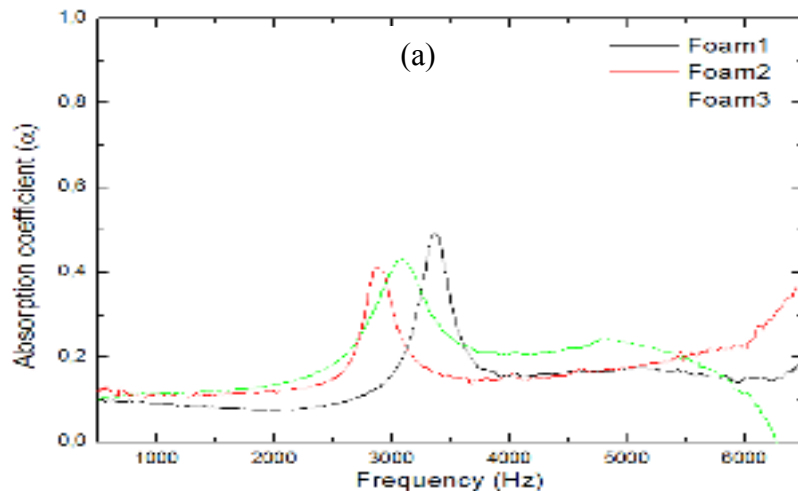


23 wt.% @ Freezer



Crystallization of PLA

PLA foams



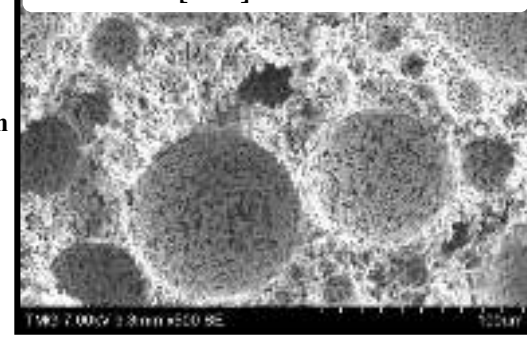
Thickness:
Porosity: 88%
Average pore size: 10.3 nm
Comp. modulus: 14 MPa
Density: 0.14g/cm³

Foam1 : [L-L] 18 wt.% @ 23°C



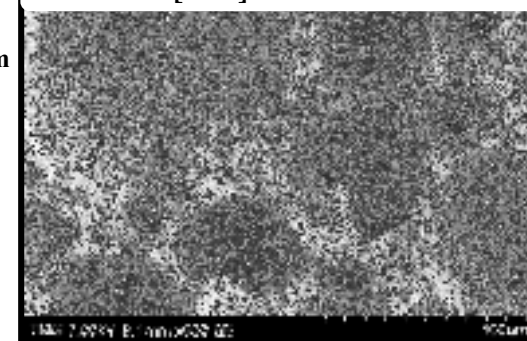
Thickness:
Porosity: 86%
Average pore size: 15.4 nm
Comp. modulus: 3.5 MPa
Density: 0.17g/cm³

Foam2: [S-L] 13 wt.% @ 23°C



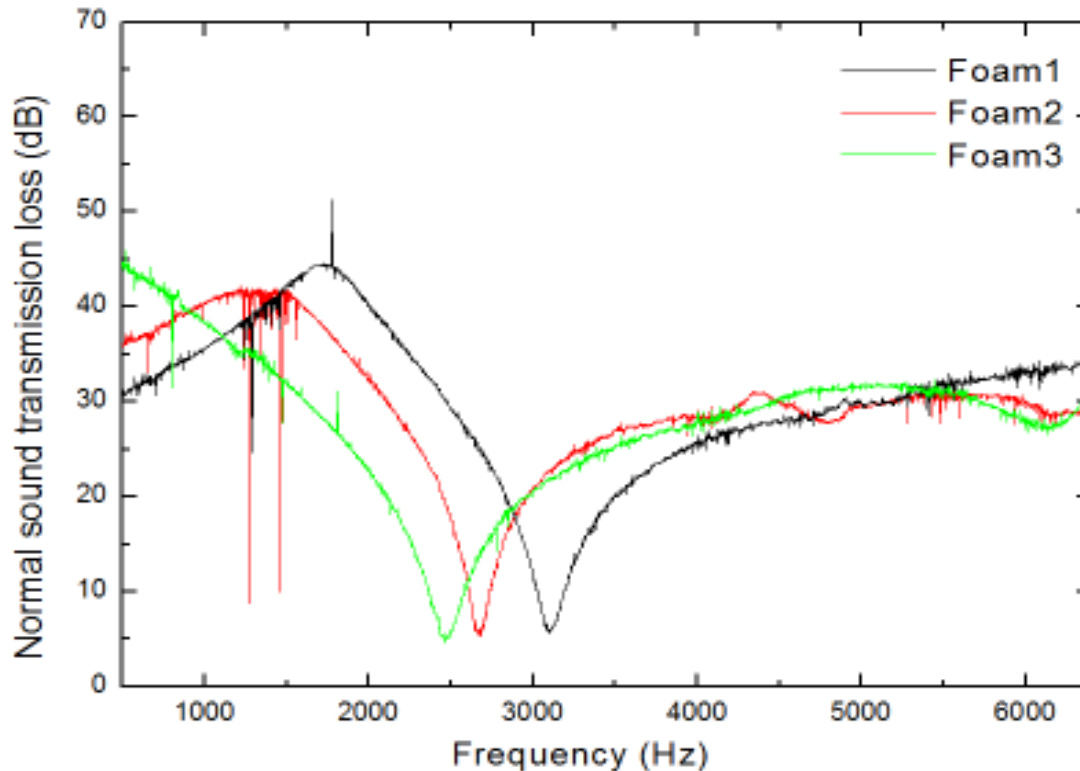
Thickness:
Porosity: 91%
Average pore size: 12.7 nm
Comp. modulus: 1,8 MPa
Density: 0.12g/cm³

Foam3: [L-L] 18 wt.% @ - 23°C



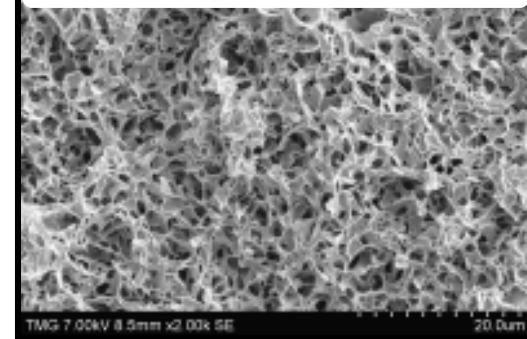
Resonance-like acoustic absorption (3000Hz and 3500Hz)

PLA foams

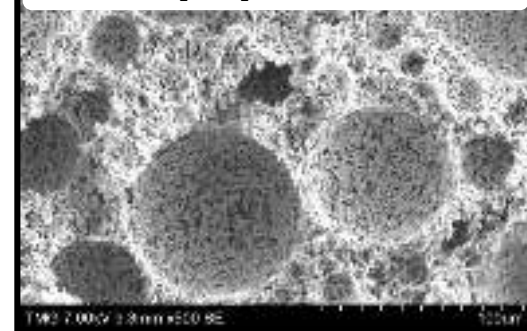


- Interesting transmission capabilities at low frequency
- Can be used as absorbing material and sound barrier

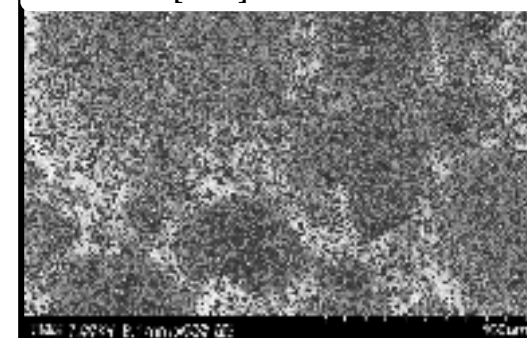
Foam1 : [L-L] 18 wt.% @ 23°C



Foam2: [S-L] 13 wt.% @ 23°C



Foam3: [L-L] 18 wt.% @ - 23°C



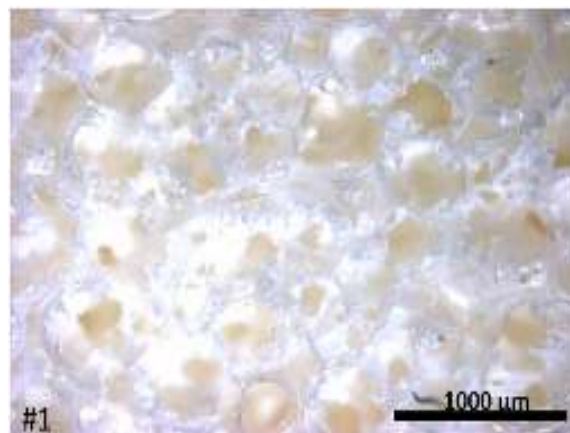
Thermoset foams

Innovative process to produce thermoset foams

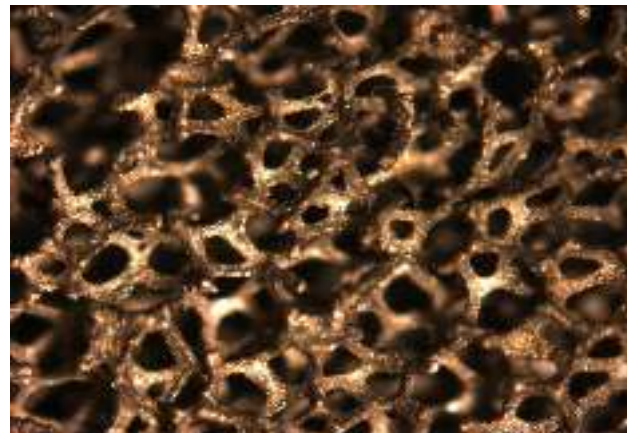
- Simple and flexible
- Cost effective
- Fully controllable



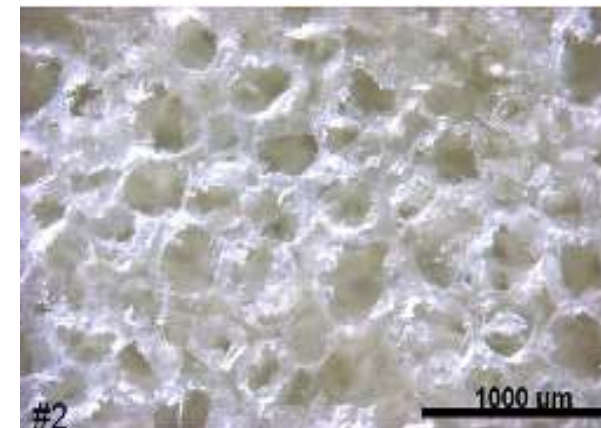
- Porosity greater than 85 % (ideal for acoustic treatment)
- Improved mechanical properties (up to 50 MPa compressive modulus)
- Porosity gradient through the thickness (ideal for non-locally acoustic treatment)
- Easy integration to composite structures (e.g. sandwich structures)



Foam #1

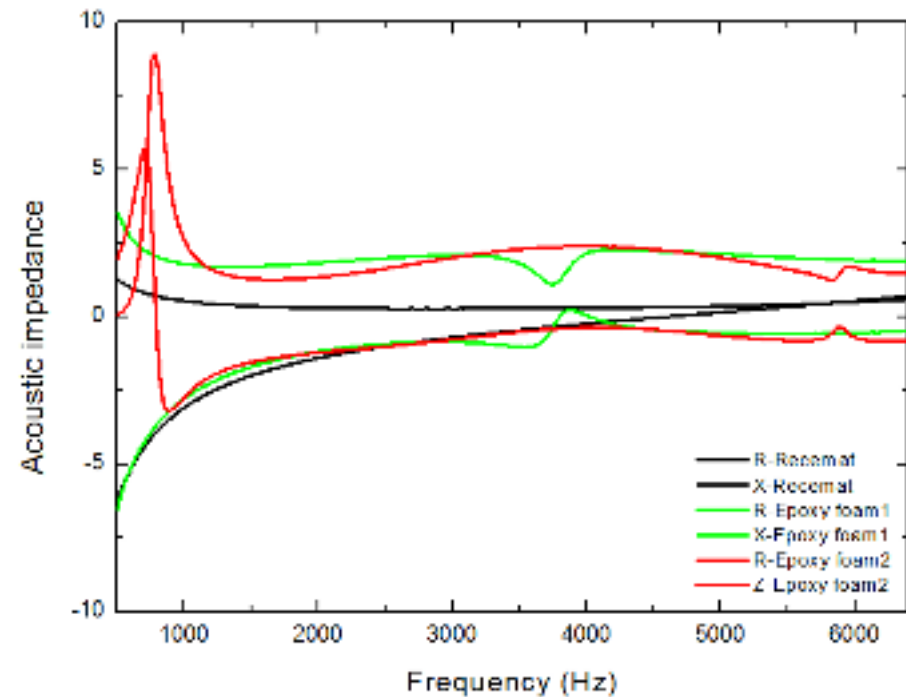
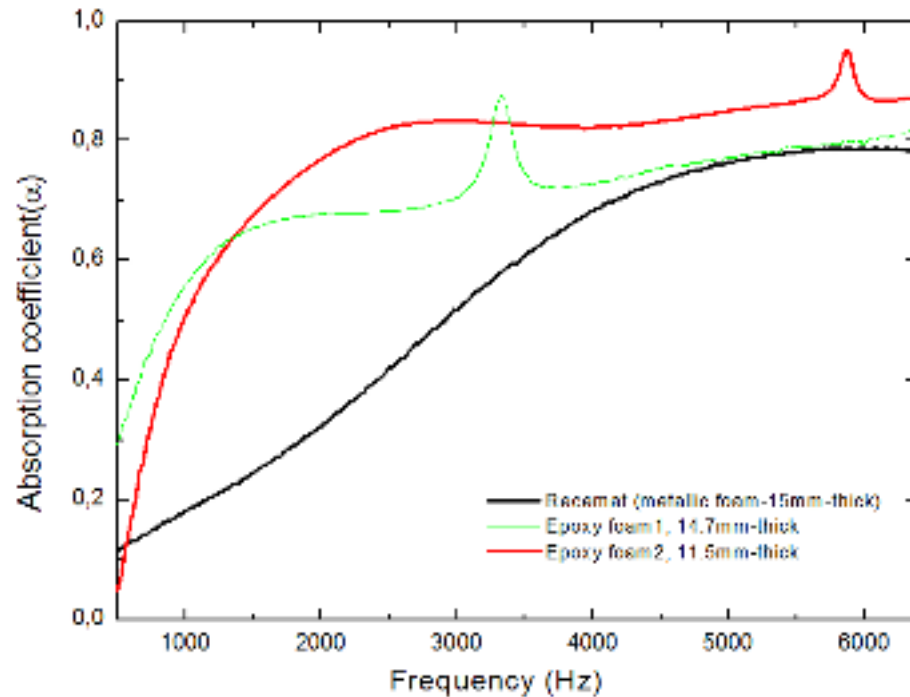


Commercial metallic foam (Recemat)



Foam #2

Thermoset foams



- Epoxy foam slightly more resistive than the metallic foam
- Absorption on a broad frequency range for epoxy foam

Characterization and modelling

Concept of equivalent fluid

$$\Delta p + \omega^2 \frac{\tilde{\rho}_{eq}}{\tilde{K}_{eq}} p = 0$$

JCA model

$$\tilde{\rho}_{eq} = \frac{\alpha_{\infty} \rho_0}{\phi} \left[1 + \frac{\sigma \phi}{j \omega \rho_0 \alpha_{\infty}} \sqrt{1 + j \omega \frac{4 \alpha_{\infty}^2 \eta \rho_0}{\sigma^2 \Lambda^2 \phi^2}} \right]$$

$$\tilde{K}_{eq} = \frac{\gamma P_0}{\phi} \frac{1}{\gamma - (\gamma - 1) \left[1 - j \frac{8 \kappa}{\Lambda'^2 C_p \rho_0 \omega} \sqrt{1 + j \omega \frac{\Lambda'^2 C_p \rho_0}{16 \kappa}} \right]^{-1}}$$

Characteristic impedance	$\tilde{Z}_c = \sqrt{\tilde{\rho}_{eq} \tilde{K}_{eq}}$
Wave number	$\tilde{k} = \omega \sqrt{\frac{\tilde{\rho}_{eq}}{\tilde{K}_{eq}}}$
Normal surface impedance	$Z = -j \tilde{Z}_c \cot(\tilde{k} e)$
Absorption coefficient	$\alpha = 1 - \frac{\tilde{Z} - Z_0}{\tilde{Z} + Z_0}$

5 parameters to be characterized ($\phi, \sigma, \alpha_{\infty}, \Lambda, \Lambda'$)

Direct method (experimental)

- Impedance tube (α, Z)
- Resistivity meter (σ)
- Porosity meter (ϕ)
- Tortuosity meter ($\alpha_{\infty}, \Lambda, \Lambda'$)

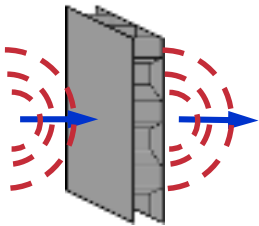
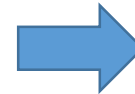
Inverse method

Comparing the model with experimental values of acoustic absorption and acoustic impedance



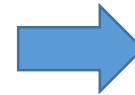
Implement mechanical damping solutions

- Lightweight
- Non intrusive
- High performance
- Cost effective



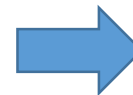
Implement sound barrier solutions

- Lightweight
- Non intrusive
- High performance
- Cost effective

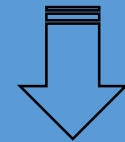


Implement acoustic absorption solutions

- Lightweight
- Non intrusive
- High performance
- Cost effective



Implement functionalities
to
existing structures
at the
design stage



Innovative concepts
No corrective patches !

